

①

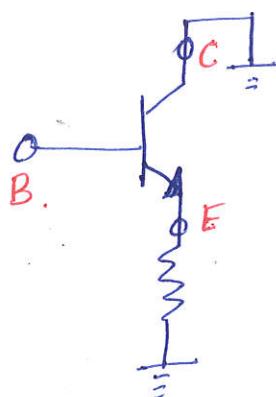
Tutorial problems

Chapter #3.

- ① An Input Voltage of 2 V_{rms} [Measured from base to ground] is applied to the circuit below. Assuming that the emitter voltage follows the base voltage exactly and that $V_{\text{BE}} (\text{rms}) = 0.1 \text{ V}$, calculate the circuit voltage amplification [$A_v = V_o/V_i$] and Emitter current for $R_E = 1 \text{ k}\Omega$ to find

$$A_v = ?$$

$$I_E = ?$$



Solutions

Using KVL

$$V_B - V_{\text{BE}} - V_E = 0$$

$$2 - 0.1 - I_E R_E = 0$$

$$I_E = 1.9 / 1000 = 1.9 \text{ mA}$$

$$V_E = I_E R_E$$

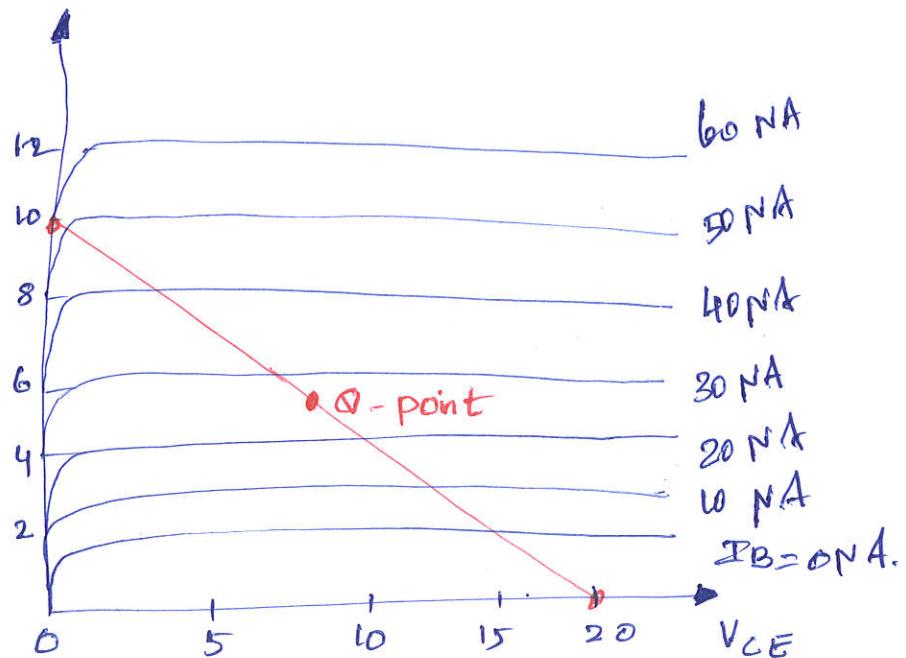
$$V_E = [1.9 \text{ mA}] [1000]$$

$$V_E = 1.9 \text{ V}$$

$$V_O = V_E$$

$$A_v = \alpha = 1.9 / 2 = 0.95$$

② Given the load line below and the defined Q-point, determine the required values of V_{CC} , R_C , and R_B for a fixed bias configuration.



From above load characteristics,

$$V_{CE} = V_{CC} = 20V \text{ at } I_C = 0 \text{ mA}$$

$$I_C = \frac{V_{CC}}{R_C} \text{ at } V_{CE} = 0V$$

$$R_C = \frac{V_{CC}}{I_C} = \frac{20V}{10 \text{ mA}} = 2 \text{ k}\Omega$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

$$R_B = \frac{V_{CC} - V_{BE}}{I_B} / I_B = \frac{20V - 0.7V}{25 \text{ mA}} = 772 \text{ k}\Omega$$

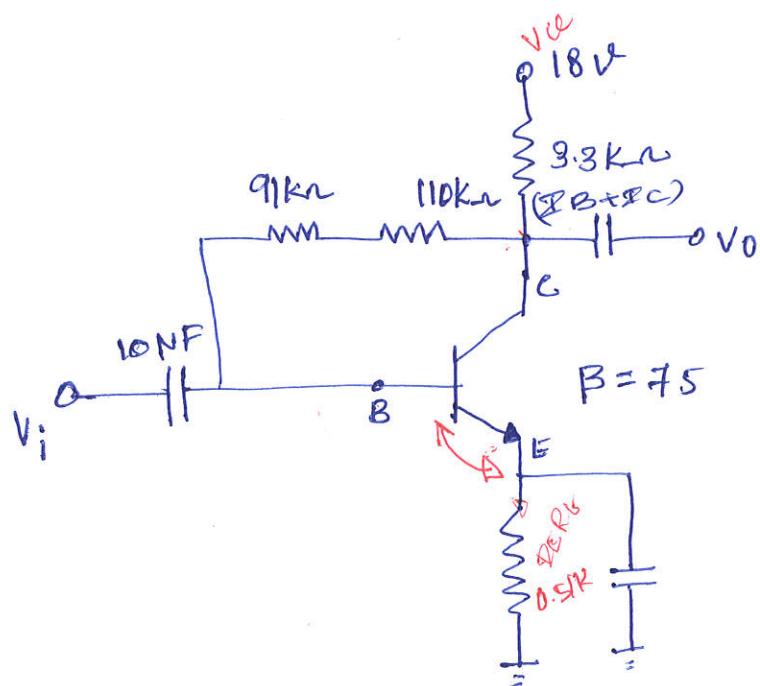
Solutions

$$V_{CC} = 20V$$

$$R_C = 2 \text{ k}\Omega$$

$$R_B = 772 \text{ k}\Omega$$

③ Determine the d.c. level of I_B and v_c for the network in figure below.



Solutions

In this case, the base resistance for the dc analysis is composed of two resistors with a capacitors connected from their ins to ground. The capacitors assumes the open circuit equivalence and $R_B = R_1 + R_2$.

Solving for I_B .

From K.V.L.

$$V_{CC} - 3.3k\Omega (I_B + I_C) - I_B (R_1 + R_2) = -V_{BE} - I_E R_E = 0.$$

But

$$I_E = I_B + I_C$$

$$I_C = \beta I_B$$

$$R_B = R_1 + R_2$$

Thus,

$$\rightarrow V_{CC} - 3.3k\Omega (I_B + \beta I_B) - I_B \underbrace{(R_1 + R_2)}_{R_B} - V_{BE} - (I_B + \beta I_B) R_E = 0$$

$$\rightarrow V_{CC} - 3.3k\Omega (I_B + \beta I_B) - I_B R_B - V_{BE} - (I_B + \beta I_B) R_E = 0$$

$$\rightarrow V_{CC} - 3.3k\Omega I_B (1 + \beta) - I_B R_B - V_{BE} - I_B (1 + \beta) R_E = 0$$

Simplifying,

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (1 + \beta)(3.3k\Omega + R_E)}$$

$\beta = 75$

$$I_B = \frac{18 - 0.7}{[91k\Omega + 110k\Omega] + [1 + 75] [8.3k\Omega + 0.51k\Omega]}$$

$$I_B = \frac{17.3V}{490.56\Omega} = 35.266NA$$

$$I_B = 35.266NA$$

Thus

$$I_C = \beta I_B$$

$$I_C = [75] [35.266 \text{ mA}]$$

$$I_C = 2.645 \text{ mA}$$

Solving for V_C .

From K.V.L.

$$V_C = 18 - 3.3k\Omega (I_B + I_C)$$

$$V_C = 18 - 3.3k\Omega (2.645 \text{ mA} + 35.266 \text{ mA})$$

$$V_C = 18 - 3.3k\Omega [2.68 \text{ mA}]$$

$$V_C = 18 - 8.845 \text{ V}$$

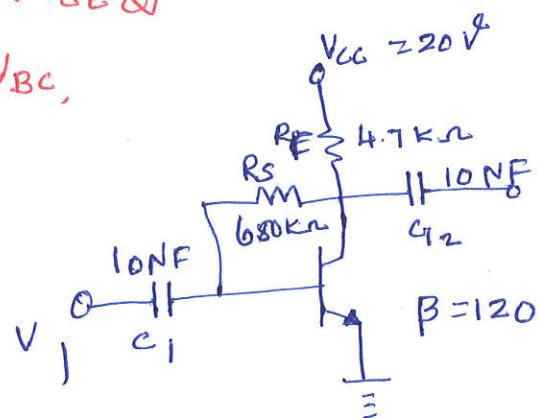
$$\boxed{V_C = 9.155 \text{ V}}$$

4. for the network of figure below.

*

a) Determine I_{CQ} and V_{GEQ}

b) find V_B , V_C , V_E , and V_{BC} ,



The absence of R_E reduces the reflection of resistive levels to simply that of R_C and equation for I_B reduce to.

Using KVL

$$V_{CC} - [I_B + I_C] R_C - I_B R_B - V_{BE} = 0$$

And

$$1 + \beta = 120 + 1 \\ = 121$$

$$I_C = \beta I_B$$

$$20 - [I_B + \beta I_B] 4.7k\Omega - I_B [680k\Omega] - 0.7 = 0$$

$$I_B = \frac{19.3}{121[4.7k\Omega] + 680k\Omega}$$

$$I_B = 15.456 \text{ mA}$$

$$I_{CQ} = \beta I_B$$

$$I_{CQ} = 120 [15.456 \text{ mA}]$$

$$I_{CQ} = 1.85 \text{ mA}$$

$$V_{CEQ} = 20 - [I_{CQ} + I_B] [4.7]$$

4,

$$V_{CEQ} = 20 - [1.85mA + I_E] [4.7k\Omega]$$

$$V_{CEQ} = 20 - [1.85mA + 15.456\mu A] [4.7k\Omega]$$

$$V_{CEQ} = 11.23V$$

Solving Base Voltage using KVL.

$$V_B - V_{BE} = 0$$

$$V_B = 0.7V$$

$$V_G = V_{CEQ} = 11.23V$$

$$V_E = 0$$

$$V_{BC} = V_B - V_G$$

$$V_{BC} = 0.7 - 11.23,$$

$$V_{BC} = -10.53V$$

 Solutions.

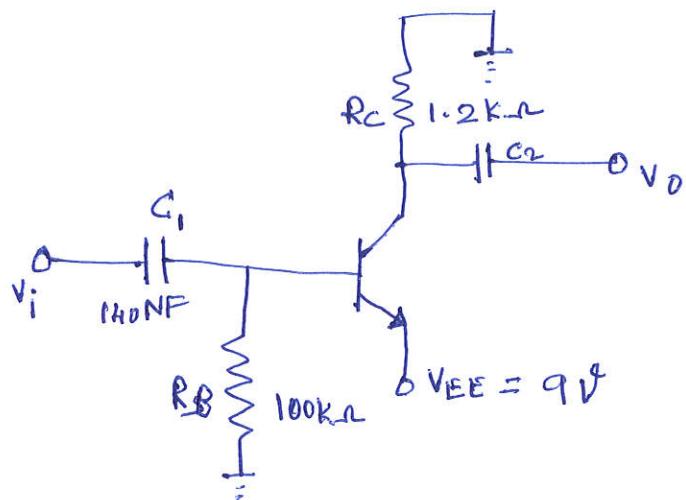
$$I_B = 15.456\mu A$$

$$V_{CEQ} = 11.23V$$

$$V_C = 11.23V$$

$$V_{BC} = -10.53V$$

⑤ Determine V_C and V_B for the network of figure below.



$$-I_B R_B - V_{BE} + V_{EE} = 0$$

$$I_B = \frac{V_{EE} - V_{BE}}{R_B}$$

$$I_B = \frac{9V - 0.7V}{100k\Omega}$$

$$= \frac{8.3V}{100k\Omega}$$

$$I_B = 83\text{ nA.}$$

$$I_C = B I_B$$

$$= [H_5] [83\text{ nA}]$$

$$I_C = 3.735 \text{ mA.}$$

5.

$$V_C = -I_C R_C$$

$$= -[3.735 \text{ mA}] [1.2 \text{ k}\Omega]$$

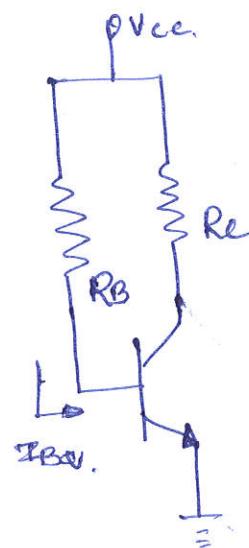
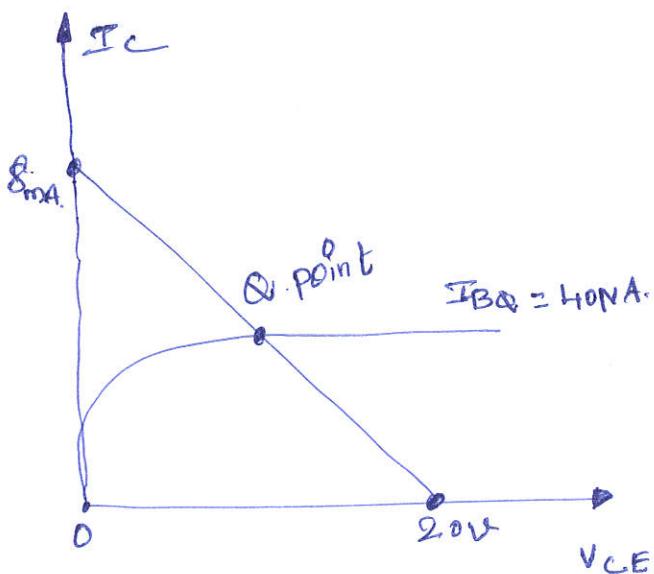
$$V_C = -4.48 \text{ V}$$

$$V_B = -I_{BRB}$$

$$= -[83 \text{ NA}] [100 \text{ k}\Omega]$$

$$V_B = -8.3 \text{ V}$$

- 6] Given the device characteristics and the fixed bias configuration from the figure below, determine V_{CC} , R_B , and R_C .



$V_{CC} = 20V$ from the load line

$$I_C = \frac{V_{CC}}{R_C}$$

$$\left| V_{CE} = 0V \right.$$

$$R_C = \frac{V_{CC}}{I_C} = \frac{20V}{8mA} = 2.5k\Omega$$

wkt

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

$$R_B = \frac{V_{CC} - V_{BE}}{I_B}$$

$$R_B = \frac{20V - 0.7V}{40mA}$$

$$R_B = \frac{19.3V}{40mA}$$

$$R_B = 482.5k\Omega \quad \boxed{\text{Ans.}}$$

6.

7) Given $\beta = 120$ and $I_E = 3.2 \text{ mA}$ for a Common-Emitter configuration with $R_o = \infty \Omega$, determine

- a) Z_i
- b) A_v if a load of $2 \text{ k}\Omega$ is applied
- c) A_i with the $2 \text{ k}\Omega$ load.

$$\text{a). } r_c = \frac{26 \text{ mV}}{I_E} = \frac{26 \text{ mV}}{3.2 \text{ mA}} = 8.125 \Omega \quad //$$

$$\text{and } Z_i = \beta r_c = [120][8.125 \Omega]$$

$$Z_i = 975 \Omega$$

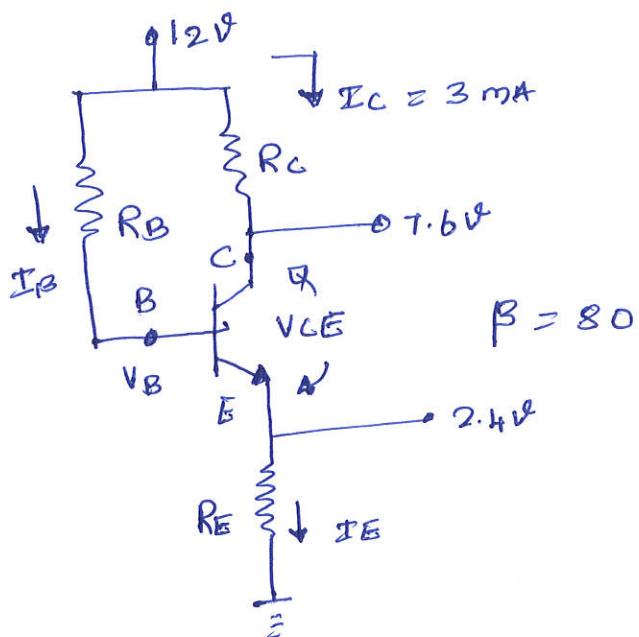
$$\text{b) } A_v = \frac{-R_L}{r_e}$$

$$= \frac{-2 \text{ k}\Omega}{8.125 \Omega}$$

$$A_v = -246.15$$

$$\text{c) } A_i = \frac{I_o}{I_i} = \beta = 120. \quad A_i = 120$$

8) For given circ. determine.



determine

- R_C
- R_E
- R_B
- V_{CE}
- V_B

Given

$$I_C = 3\text{mA}$$

$$V_C = 7.6\text{V}$$

$$V_E = 2.4\text{V}$$

$$\beta = 80$$

$$V_{CC} = 12\text{V}$$

PF.

Solutions

e) $V_B = ?$

$$V_{BE} = 0.7V \quad [\text{Si}]$$

$$V_B - V_E = 0.7V$$

$$V_B = 2.4V + 0.7V$$

$$V_B = 3.1V$$

d) V_{CE}

$$V_{CE} = V_C - V_E$$

$$= 7.6V - 2.4V$$

$$V_{CE} = 5.2V$$

c) R_B

Apply KVL in input loop

$$V_{CC} - I_B R_B = V_B$$

$$+12V - I_B R_B = V_B$$

$$+12V - I_B R_B = 3.1V$$

$$I_B = \frac{I_C}{\beta}$$

$$= \frac{3 \text{ mA}}{80}$$

$$I_B = 37.54 \text{ nA}$$

$$R_{BE} = \frac{12V - 3.1V}{37.54 \text{ nA}}$$

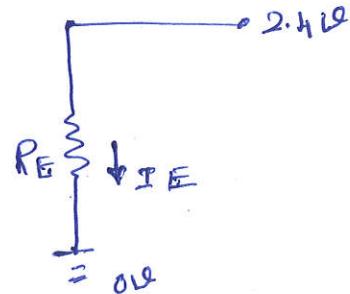
$$R_B = \frac{12V - 3.1V}{37.5 \text{ nA}}$$

$$R_B = 237.4 \text{ k}\Omega$$

5] RE

Apply KVL in RE loop

$$2.4V - I_E R_E = 0V$$



$$\therefore I_E = I_C$$

$$\frac{2.4V}{3 \text{ mA}} = R_E$$

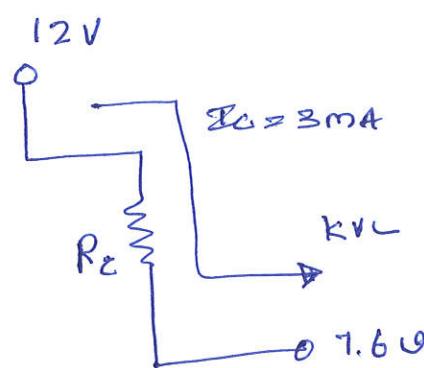
$$R_E = 0.8 \text{ k}\Omega$$

a) R_C

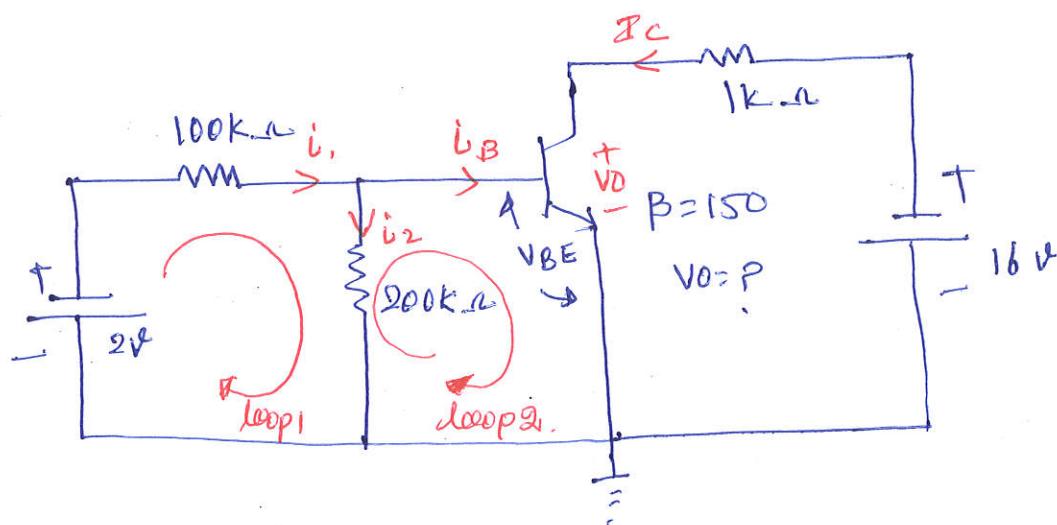
$$12V - I_C R_C = 7.6V$$

$$R_C = \frac{12V - 7.6V}{3mA}$$

$$R_C = 1.47 k\Omega$$



q] Analysis given circuit. find $V_O = ?$



Given

$$\beta = 150$$

$$V_{BE} = 0.7V$$

Relations.

$$I_C = \alpha I_E$$

$$I_C = \beta I_B$$

$$I_E = [1 + \beta] I_B$$

$$① \text{ KCL} \quad i_1 = i_2 + I_B$$

$$② \text{ KCL} \rightarrow i_1(100k) + i_2(200k) - 2V = 0 \rightarrow \text{Loop 1}$$

$$-i_2(200k) + V_{BE} = 0 \quad \text{loop 2}$$

$$V_{BE} = i_2(200k)$$

$$\frac{V_{BE}}{200k} = i_2$$

$$i_2 = \frac{0.7}{200k}$$

$$i_2 = 3.5 \text{ mA}$$

Now Sub i_2 value in loop 1

$$i_1(100k) + 3.5 \text{ mA}(200k) - 2V = 0$$

$$i_1(100k) = \frac{2 - (3.5 \text{ mA})(200k)}{2 - (3.5 \text{ mA})(200k)}$$

$$i_1 = \frac{2 - (3.5 \text{ mA})(200k)}{100k}$$

$$i_1 = 13 \text{ mA}$$

③ Now Apply i_1 & i_2 Value in KCL equation.

$$i_1 = i_2 + I_B$$

$$13 \text{ mA} = 3.5 \text{ mA} + I_B$$

$$I_B = 9.5 \text{ mA}$$

$$I_B = 13 \text{ mA} - 3.5 \text{ mA}$$

(9)

Now we find $I_C = ?$

$$I_C = \beta I_B$$

$$I_C = 150 \times 9.5 \text{ mA}$$

$$I_C = 0.001425$$

Now we find V_O using ohms law.

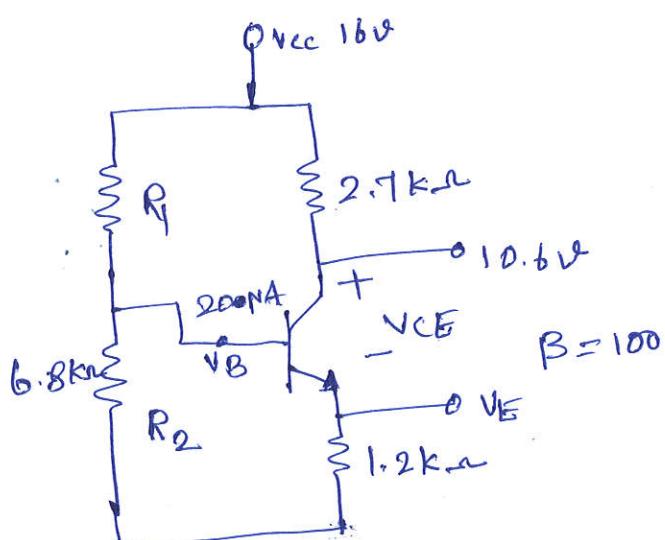
$$16 - V_O = (0.001425)(1k)$$

$$V_O = 16 - (0.001425)(1k)$$

$$V_O = 14.575 \text{ V}$$

(10) Determine and analysis

- a) I_C b) V_E c) V_{CC} d) V_{CE} e) V_B f) R_I .



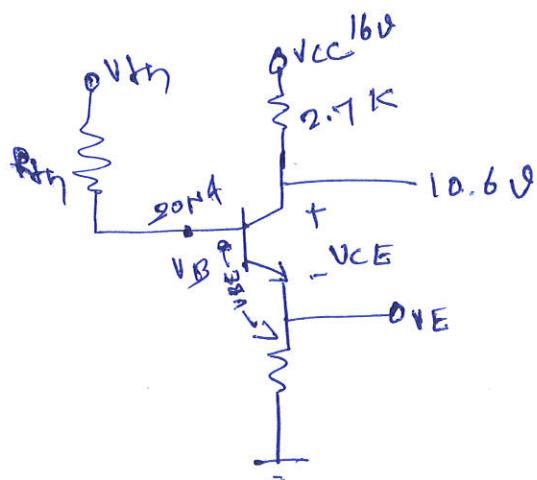
Given

$$I_B = 20 \text{ nA}, V_C = 10.6 \text{ V}, R_C = 2.7 \text{ k}\Omega, R_2 = 6.8 \text{ k}\Omega$$

$$R_C = 2.7 \text{ k}\Omega, B = 100, R_E = 1.2 \text{ k}\Omega$$

Solutions

Now we can draw Thevenin equivalent ckt



$$V_{th} = \frac{V_{CC} R_2}{R_1 + R_2}$$

$$R_m = \frac{R_1 R_2}{R_1 + R_2}$$

a) $I_C = ?$

$$I_C = B I_B$$

$$I_C = 100 \times 200 \text{ nA}$$

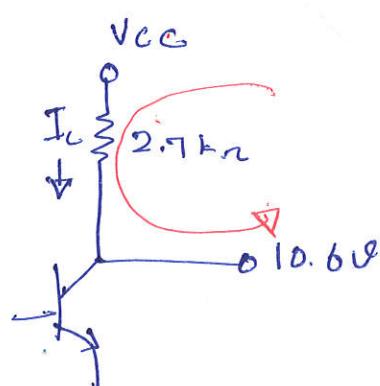
$I_C = 2 \text{ mA}$

c) $V_{CC} = ?$

$$V_{CC} - I_C R_C = 10.6 \text{ V}$$

$$V_{CC} = 10.6 + (2 \text{ mA}) (2.7 \text{ k}\Omega)$$

$V_{CC} = 16 \text{ V}$



$$b) V_E = ?$$

kT

$$I_E = I_C + I_B$$

I_B is very small

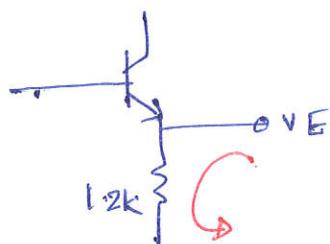
∴

$$I_E \approx I_C$$

$$I_E = 2 \text{ mA} + 20 \text{nA}$$

$$= 2 \text{ mA} + 0.02 \text{ mA}$$

$$\boxed{I_E = 2.02 \text{ mA}} \rightarrow \text{Reason } I_E \approx I_C$$



$$V_E - I_E R_E = 0$$

$$V_E = I_E R_E$$

$$V_E = (2.02 \text{ mA})(1.2 \text{ k}\Omega)$$

$$\boxed{V_E = 2.42 \text{ mV}}$$

$$d) V_{CE} = ?$$

$$V_{CE} = V_C - V_E$$

$$V_{CE} = 10.6 \text{ V} - 2.42 \text{ mV}$$

$$\boxed{V_{CE} = 8.176 \text{ V}}$$

$$e) V_B = ?$$

$$V_{BE} = V_B - V_E$$

$$0.7 = V_B - 2.124 \text{ V}$$

$$V_B = 3.124 \text{ V}$$

$$f) R_1 = ?$$

→ potential point

$$V_{th} \approx V_B$$

$$V_{th} = \frac{V_{CC} R_2}{R_1 + R_2}$$

$$V_{th} = \frac{16 \times 6.8}{R_1 + 6.8 \text{ k}\Omega}$$

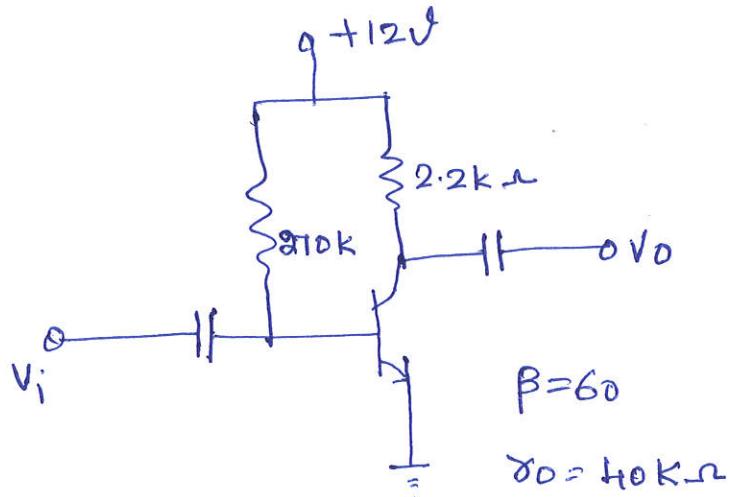
$$V_{th} \approx V_B$$

$$3.12 \text{ V} = \frac{16 \times 6.8}{R_1 + 6.8 \text{ k}\Omega}$$

$$R_1 = 28 \text{ k}\Omega$$

11.

for the network shown,



- i) Determine Z_i and Z_o
- ii) Determine Voltage gain
- iii) Determine Current gain.

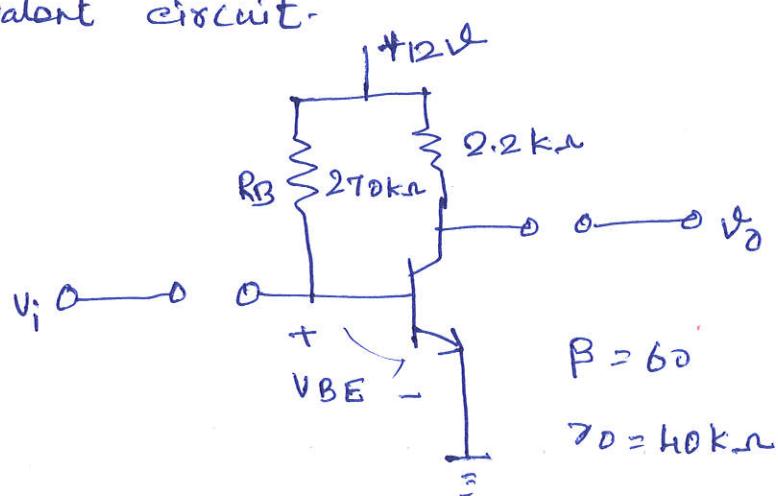
Solutions

$$R_B = 270\text{k}\Omega \quad \beta = 60$$

$$R_C = 2.2\text{k}\Omega \quad Z_o = 40\text{k}\Omega$$

$$\gamma_e = \frac{26\text{mV}}{I_E}$$

D.c. equivalent circuit.



an applying K.V.L \rightarrow Input loop

$$-12\text{V} - I_B R_B + V_{BE} = 0\text{V}$$

$$I_B = \frac{12V - 0.7V}{270\text{ k}\Omega}$$

$$I_B = 0.04185 \text{ mA} = 41.85 \text{ nA.}$$

Calculate I_E .

$$I_E = I_C + I_B$$

$$= \beta I_B + I_B = [\beta + 1] I_B$$

$$I_E = 61 \times 41.85 \text{ nA}$$

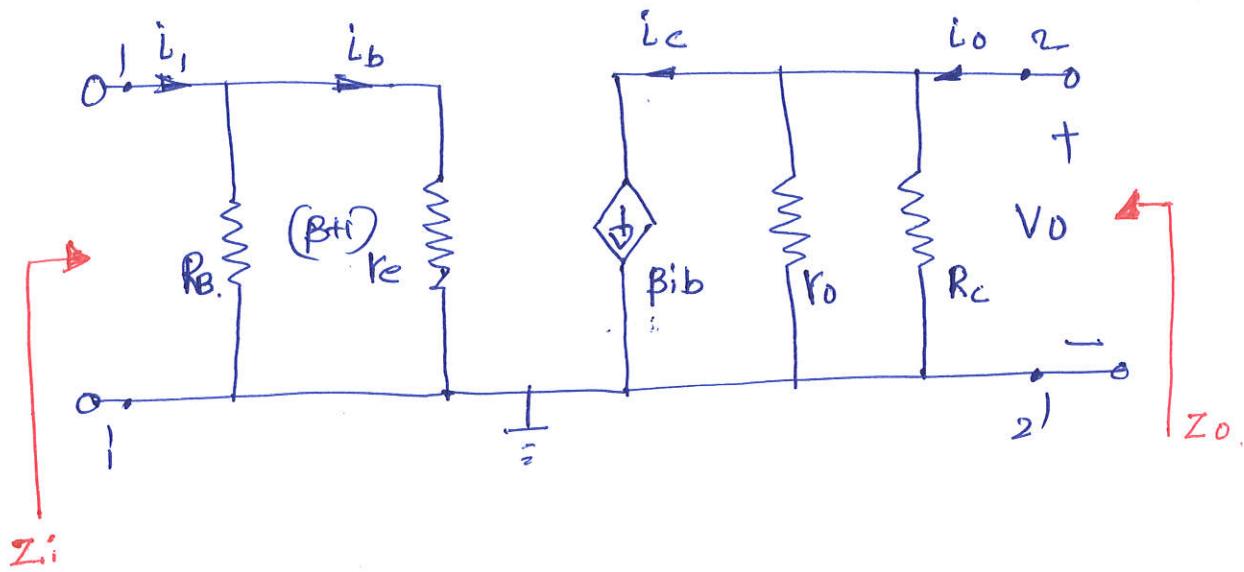
$$I_E = 2552.85 \text{ nA} = 2.553 \text{ mA.}$$

$$r_e = ?$$

$$r_e = \frac{26 \text{ mV}}{2.553 \text{ mA.}}$$

$$r_e = 10.18 \Omega$$

To find Z_i and Z_o to obtain A.C. equivalent circuit.



Z_i

$$Z_i = R_B \parallel (\beta + i)\gamma_e$$

$$(\beta + i)\gamma_e = 0.621 \text{ k}\Omega$$

$$= \frac{R_B \cdot (\beta + i)\gamma_e}{R_B + (\beta + i)\gamma_e}$$

$$Z_i = \frac{(270 \text{ k}\Omega)(0.621 \text{ k}\Omega)}{270 \text{ k}\Omega + 0.621 \text{ k}\Omega}$$

$$\underline{R_B \geq 10(\beta + i)\gamma_e}$$

$$Z_i = (\beta + i)\gamma_e$$

$$= 0.6195 \text{ k}\Omega$$

$$\boxed{Z_i = 619.5 \Omega}$$

$$\boxed{Z_i = 619.5 \Omega}$$

Z_o

$$Z_o = R_o \parallel R_C$$

$$Z_o = 40 \text{ k}\Omega \parallel 2.2 \text{ k}\Omega$$

$$\boxed{Z_o = 2.085 \text{ k}\Omega}$$

$$A_V = \frac{V_O}{V_I} = \frac{-\beta i_B R_C}{I_B (B+A) r_e}$$

$B+1 \approx B$

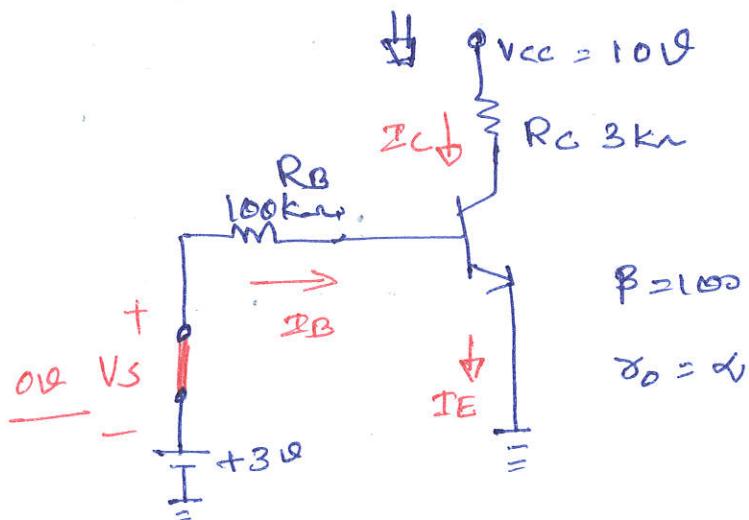
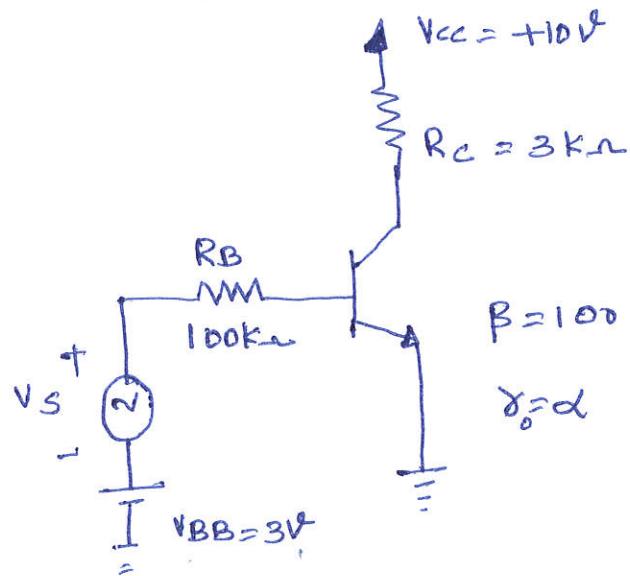
$$A_V = \frac{-R_C}{r_e} = \frac{2.2 \text{ k}\Omega}{10.18 \text{ }\Omega$$

$A_V = -216.1$

$$A_i = \frac{i_o}{i_i} = 60.$$

current gain $A_i = \beta = 60$.

1) Determine the ~~Voltage gain~~ of the amplifier shown in figure.



Apply KVL Input Side.

$$V_{BE} = 0.7V$$

$$0V + 3V - (100k)\text{I}_B - V_{BE} = 0$$

$$\text{I}_B = \frac{3V - 0.7V}{100k}$$

$$\text{I}_B = 0.023\text{mA} \text{ or } \underline{\underline{23\text{nA}}}$$

$$I_C = \beta I_B$$

$$I_C = 23mA \times 100$$

$$I_C = 2.3mA$$

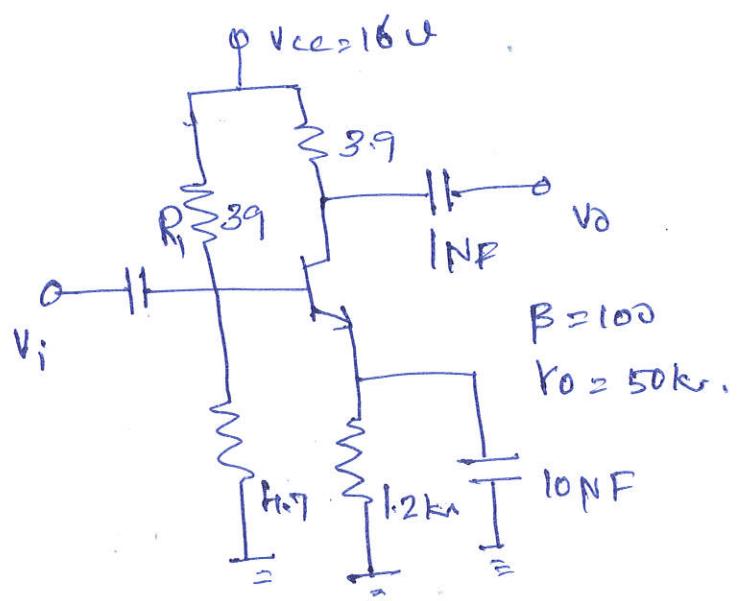
For network shown in figure.

a) Determine r_c

b) calculate Z_i and Z_o

c) find A_V

d) find A_I .



Solutions

$$r_c = \frac{26mV}{I_E}$$

$$R_i = 3.9k, R_2 = 4.7k, R_C = 3.9k, R_E = 1.2k$$

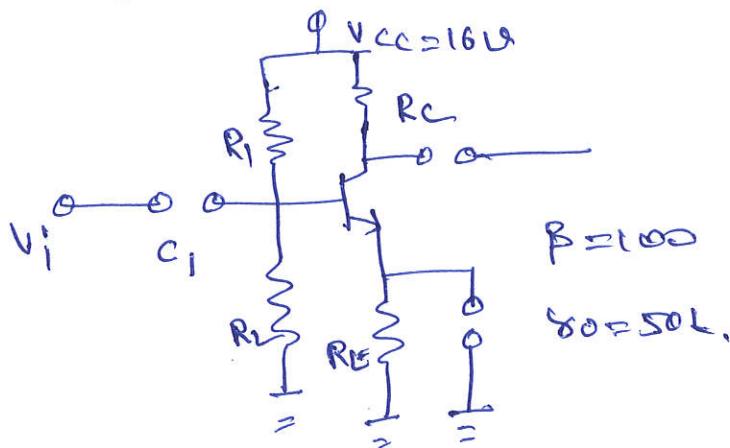
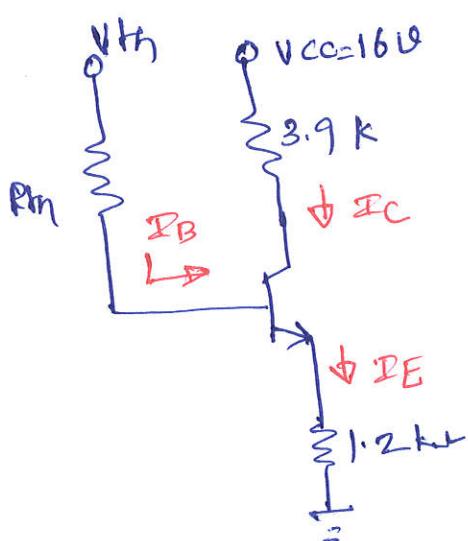
$$V_{CC} = 16V, C_1 = 1NF, C_2 = 1NF, C_3 = 10NF, \beta = 100$$

$$r_o = 50k\Omega$$

14.

Find $\gamma_E = ?$ We need to find I_E

D.C. equivalent circuit

Voltage divider bias $\rightarrow V_{TH}$ ckt

$$V_{TH} = \frac{R_2 \cdot V_{CC}}{R_1 + R_2}$$

~~$R_1 \parallel R_2$~~

$$R_m = R_1 \parallel R_2$$

$$V_{TH} = \frac{4.7k \times 16V}{39k + 4.7k} = 1.72V$$

$V_{TH} = 1.72V$

$$R_m = \frac{R_1 R_2}{R_1 + R_2} = 4.194k\Omega$$

Apply KVL in Input Loop

$$V_{th} - I_B R_{th} - V_{BE} - I_E (1.2k) = 0 \quad \rightarrow (B+D)I_B.$$

WKT

$$I_E = I_B + I_C$$

$$I_C = \beta I_B$$

$$I_E = (B+1)I_B$$

$$I_B = \frac{V_{th} - V_{BE}}{R_m + (B+1)(1.2k)}$$

$$I_B = \frac{1.72V - 0.7V}{4.19H_k + (101)(1.2k\Omega)}$$

$$I_B = 8.13mA$$

$$\underline{\underline{I_C = ?}}$$

$$I_C = \beta I_B$$

$$I_C = 100 \times 8.13mA$$

$$I_C = 813.4mA$$

$$I_E = 8.13mA + 813.4mA$$

$$I_E = 0.821mA$$

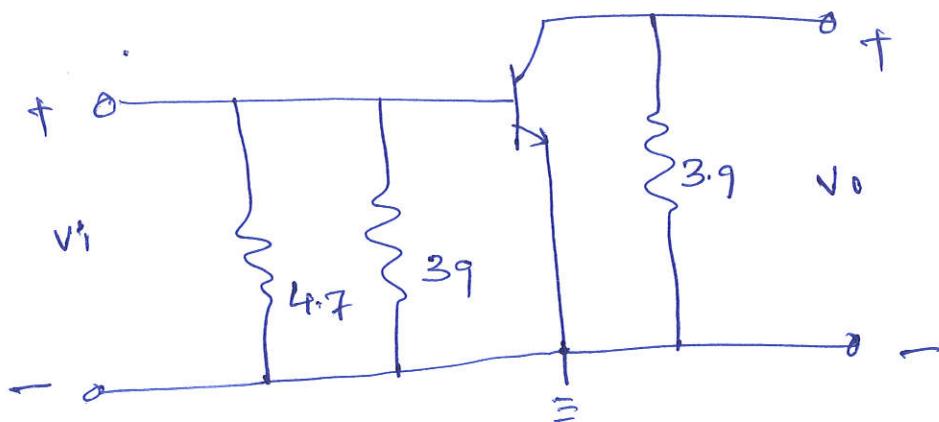
$$r_e = \frac{26 \text{ mV}}{I_E}$$

$$r_e = \frac{26 \text{ mV}}{0.82 \text{ mA}}$$

$$r_e = 31.6 \Omega$$

To the calculation Z_i and Z_o we need the equivalent circuit before AC202.

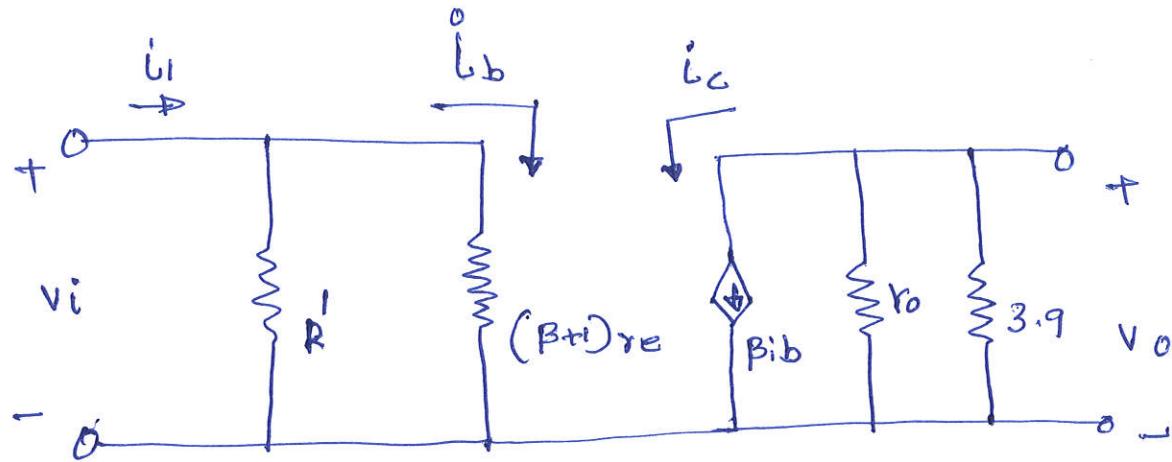
A.C. equivalent ckt.



$\Rightarrow Y_Z$ model

$$R' = 4.7 \parallel 39$$

$$R' = 4.19 \text{ k}\Omega = R_{th.}$$



$$Z_i = \frac{1}{R'_{||} [(\beta + 1)r_e]} = \frac{\frac{1}{R'} [(\beta + 1)r_e]}{R' + [(\beta + 1)r_e]} = 1.811 \text{ k}\Omega,$$

$$[(\beta + 1)r_e] = 3.19 \text{ k}\Omega$$

$$Z_o = r_o || 3.9$$

$$r_o = 50 \text{ k}\Omega$$

H.W

c) A_V

$$A_{i2} \frac{\partial I_p}{I_p}$$

d) A_i

$$A_V = \frac{R_C}{R_E} = \frac{R_C}{\gamma_e 1} = \frac{3.9}{31.6} = 0.123.$$

$$A_i = \beta =$$

JFET Solved problems.

① The device parameters for n-channel JFET are

- * Maximum drain current $[I_{DSS}] = 10\text{mA}$.
- * Pinch-off Voltage $[V_p] = -4\text{V}$

Calculate the drain current for.

- a) $V_{GS} = 0\text{V}$ b) $V_{GS} = -1\text{V}$ c) $V_{GS} = -4\text{V}$.

Solutions.

$$I_D = I_{DSS} \left[1 - \frac{V_{GS}}{V_p} \right]^2$$

Case a) $V_{GS} = 0\text{V}$ & $V_{DS} > |V_p|$

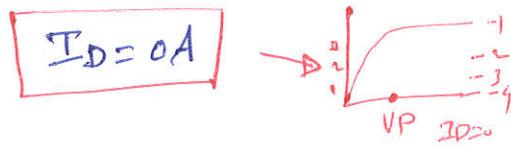
$$I_D = I_{DSS}$$

$I_D = 10\text{mA}$

Case c:

$$V_{GS} = -4\text{V}$$

$$V_p = -4\text{V} = I_D = 0$$



Case b)

$$V_{GS} = -1\text{V}$$

$$I_D = I_{DSS} \left[1 - \frac{V_{GS}}{V_p} \right]$$

$$= 10\text{mA} \left[1 - \left[\frac{-1}{-4} \right] \right]^2 = 10\text{mA} [1 - 0.25]$$

$I_D = 5.625\text{mA}$

Q2) The reverse gate voltage of JFET when changes from 4.4V to 4.2V, the drain current changes from 2.2 mA to 2.6 mA, find out the value of transconductance.

Solution

$$g_m = \frac{\partial P_i}{\partial V_D} \quad \left| \text{for constant } \partial P_i \right.$$

$$g_m = \frac{\Delta I_D}{\Delta V_{GS}} \quad \left| \begin{array}{l} \text{Change in output i} \\ \text{Change in input v} \end{array} \right. \quad \text{constant } \partial P_i$$

$$\Delta V_{GS} = 4.4V - 4.2V$$

$$= 0.2V$$

$$\Delta I_D = 2.2mA - 2.6mA$$

$$= -0.4mA$$

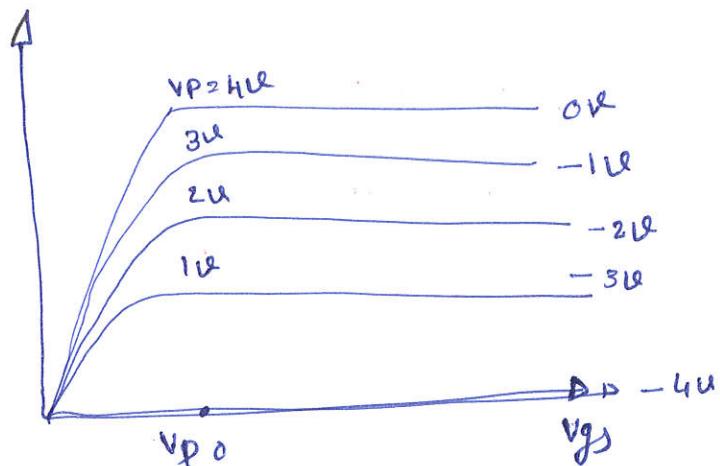
- dont want to take
→ not Required

$$g_m = \frac{0.4mA}{0.2V} = 2mA/V$$

$g_m = 2 mmbD$

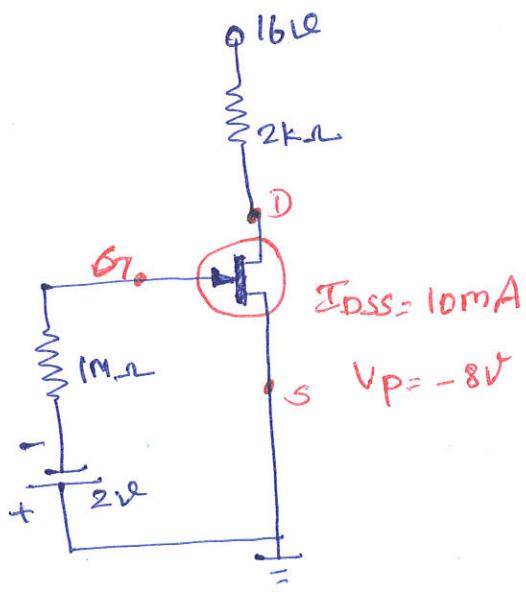
2.

2. The pinch off voltage for an n-channel JFET is 4 Volts. Then pinch off occurs for V_{DS} when $V_{GS} = -1$ Volts is.



$$V_P = 3V \text{ for } V_{GS} = -1 \text{ Volts.}$$

3. Determine the following for the network shown in figure.



a) V_{GSQ}

b) I_{DQ}

c) V_{DS}

d) V_D

e) V_G

f) V_S .

* In FET $I_G \approx 0A$

a] $\Rightarrow \alpha_{\text{pt}} = [V_{\text{DSR}}, I_{\text{DR}}]$

c] V_{DS} \rightarrow O/p Voltage

d] V_D \rightarrow potential of the drain

e) V_G \rightarrow potential of the Gate.

f) V_S \rightarrow potential at the Source

} \Rightarrow not a potential difference
 \hookrightarrow pot at a pt

$V_D =$ p.d between D and ground
↓ ↓
 V_D O/p

$$V_D = V_D - 0V = V_D - V_S$$

$$V_D = V_{D_S}$$

\rightarrow Ans of parts e & d as same

$$V_G = V_G - 0V$$

$$V_S = 0V$$

$$V_G = V_{G_S} - V_S$$

$$V_G = V_{G_S}$$

\rightarrow Ans of a part equal to the Ans of e part

already we know that

Source is connected to ground

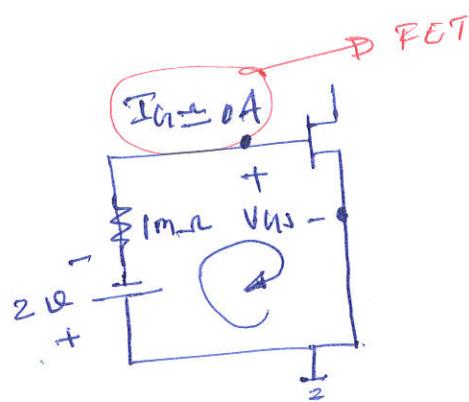
$$V_S = 0V \leftarrow \text{SO.}$$

a) V_{GSQ}

Apply KVL

$$-2V - Imz(0) - V_{GS} = 0$$

$$V_{GSQ} = -2V$$

c) $V_G = V_{GS}$

$$V_{GSQ} = V_{GQ}$$

 $wkT \rightarrow \text{Given}$

$$I_{DSS} = 10mA$$

$$V_P = -8V$$

$$b) I_D = I_{DSS} \left[1 - \frac{V_{GS}}{V_P} \right]^2$$

$$I_D = 10mA \left[1 - \frac{[-2]}{[-8]} \right]^2$$

$$d) V_D = V_{DS}$$

$$I_D = 5.62mA$$

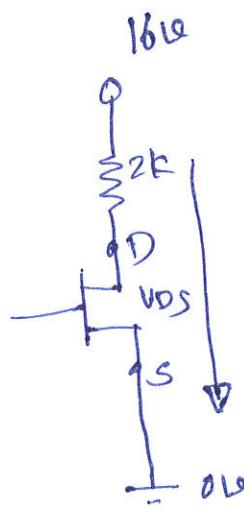
c) $V_{GS} = 0$ p voltage

Apply KVL

$$16V - I_D [2k] - V_{DS} = 0$$

$$16V - 5.62 [2k] - V_{DS} = 0$$

$$V_{DS} = 4.75V$$



$$e) V_D = 4.75V$$

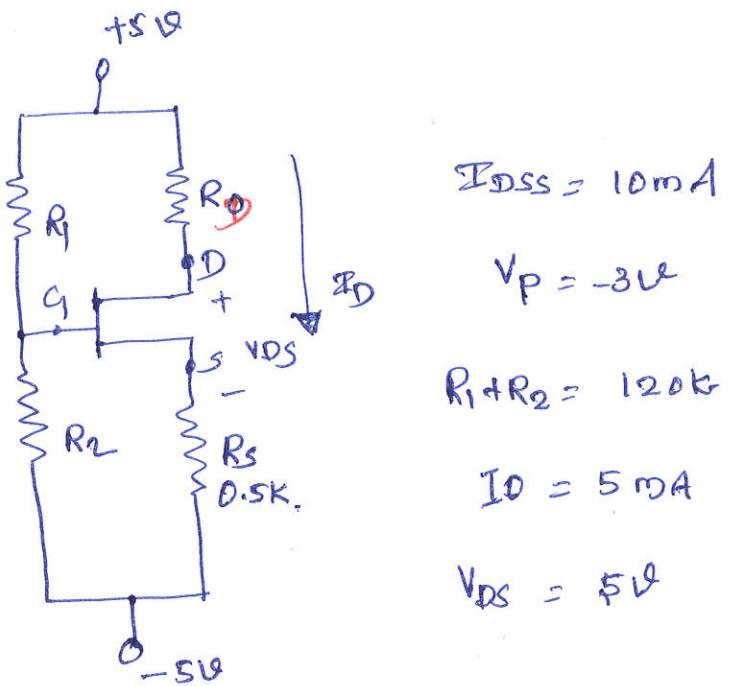
$$f) V_S = 0V$$

$$g) I_D = I_{DQ}$$

$$I_{DQ} = 5.62mA$$

3) Determine the following parameters for the network as

Shown in figure.



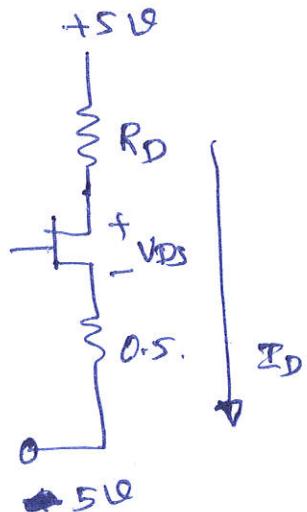
Find. R_1, R_2, R_D

Apply KVL find R_D in output

$$5 - I_D(R_D) - V_{DS} - 0.5(I_D) + 5 = 0$$

$$5 - 5 \text{ mA}(R_D) - 5 \text{ V} - 0.5(5 \text{ mA}) + 5 = 0$$

$$R_D = 0.5 \text{ k}\Omega$$



We need two eqn : 2 unknowns: R_1 & R_2 .

$$1) R_1 + R_2 = 120 \text{ k}\Omega$$

Apply Stevenion logic

$$V_G = V_G^I + V_G^{II}$$

$$V_G^I = 5V \rightarrow ON$$

$$V_{GII}^{II} = -5V \rightarrow ON$$

$$V_{GII}^I = V$$

$$V_G = 5 \cdot \frac{R_2}{R_1+R_2} - 5 \cdot \frac{R_1}{R_1+R_2}$$

$\frac{R_2}{R_1+R_2} \rightarrow$ Numerator
Connected to ground

WKT

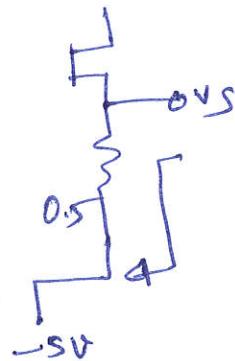
$$V_{GS} = V_G - V_S$$

$$V_G = V_{GS} + V_S$$

Apply KVL

we will get

$$\frac{V_S + 5}{0.5k} = I_D$$



$$V_S + 5 - 0.5k = 0$$

WKT

$$I_D = 5mA$$

$$V_S + 5 = 0.5k I_D$$

$$\frac{V_S + 5}{0.5k} = 5mA$$

$$\frac{V_S + 5}{0.5k} = I_D$$

$V_S = -2.5V$

Now use I_D equations we will get V_{GS}

$$I_D = I_{DSS} \left[1 - \frac{V_{GS}}{V_P} \right]^2$$

$$5mA = 10mA \left[1 - \frac{V_{GS}}{-3V} \right]^2$$

Finally we will get

$$V_{GS} = -0.87V$$

∴

$$V_G = V_{GS} + V_S$$

$$V_G = -0.87 - 2.5V$$

$$V_G = -3.37V$$

Now we can re-write two equations.

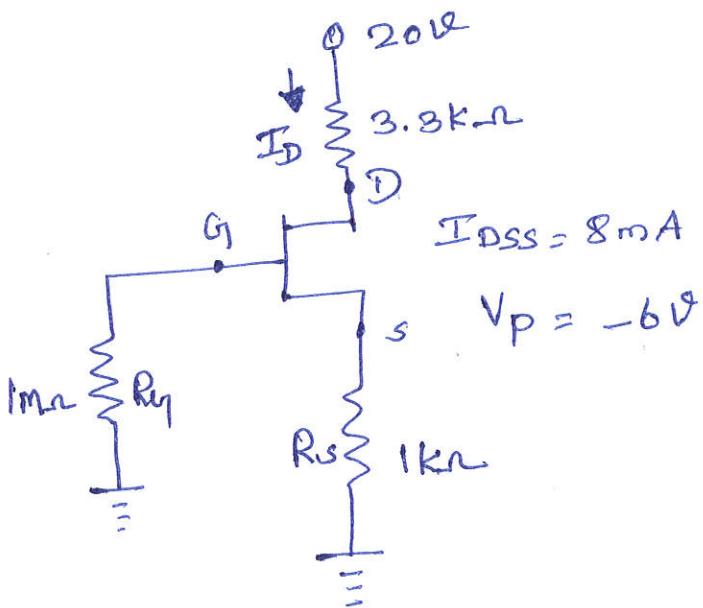
$$R_1 + R_2 = 120k\Omega \rightarrow ①$$

$$5 \cdot \frac{R_2}{R_1 + R_2} - 5 \cdot \frac{R_1}{R_1 + R_2} = -3.37k \rightarrow ②$$

Solving these two equations we will get

$$R_1 \text{ & } R_2$$

4] Determine the following for the network.



- a) V_{GS}
- b) I_D
- c) V_{DS}
- d) V_S
- e) V_G
- f) V_D .

Solutions.

a) The Gate to Source voltage.

$$V_{GS} = -I_D R_S$$

Assume $I_D = 4\text{mA}$

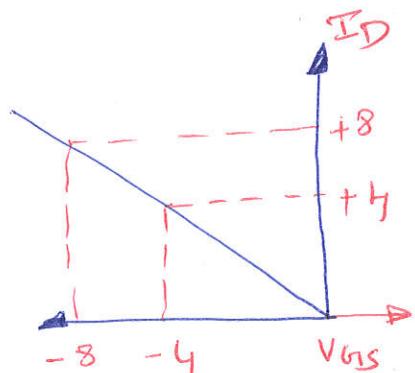
$$V_{GS} = -[4\text{mA}] [1\text{k}\Omega]$$

$V_{GS} = -4\text{V}$

$$I_D = 8\text{mA}$$

$$V_{GS} = -[8\text{mA}] [1\text{k}\Omega]$$

$V_{GS} = -8\text{V}$



From the Shockley equation.

$$V_{GS} = \frac{V_P}{2} = -3V$$

$$I_D = \frac{I_{DSS}}{4} = 2mA.$$

b) At the quiescent point

$$I_{DQ} = 2.6mA.$$

$$c) V_{DS} = V_{DD} - I_D (R_S + R_D)$$

$$= 20V - (2.6mA) (1k\Omega + 3.3k\Omega)$$

$$= 8.82V.$$

$$d) V_S = I_D \cdot R_S$$

$$= (2.6mA) (1k\Omega)$$

$$V_S = 2.6V$$

$$e) V_G = 0$$

$$f) V_D = V_{DS} + V_S = 11.42V$$

(or)

$$V_D = V_{DD} - I_D R_D = 11.42V.$$